One-Bit Delta Sigma D/A Conversion Part I: Theory

Randy Yates

mailto:randy.yates@sonyericsson.com

July 28, 2004

1			
on	tο	\mathbf{n}	
	ししし	TT	っし

1	What Is A D/A Converter?	3
2	Delta Sigma Conversion Revealed	5
3	Oversampling	6
4	Noise-Shaping	12
5	Alternate Modulator Architecture	19
6	Psychoacoustic Noise-Shaping	22
7	The Complete Modulator	25
8	References	26

1 What Is A D/A Converter?

• Rick Lyons [1] derives A/D SNR as a function of word length N and loading factor LF:

 $SNR = 6.02N + 4.77 + 20\log_{10}(LF),$

- *LF* is the "loading factor," a value representing the normalized RMS value of the input signal. For a sine wave, *LF* = 0.707. Here we ignore the constant factor of 1.77 dB and we round the *N* coefficient to 6 to simplify.
- This can be generalized to express the SNR of any N-bit amplitude-quantized transfer function and thus applies to D/A conversion as well.

For a generic D/A converter in which bandwidth, output bit-width, and other parameters may not be clearly defined, this motivates the following

Definition 1 An N-bit D/A converter converts a stream of discrete-time, linear, PCM samples of N bits at sample rate F_s to a continuous-time analog voltage with a signal-to-quantization-noise power ratio of 6N dB in a bandwidth of $F_s/2$ Hz.

This gives a basis by which we may evaluate the number of bits of any converter architecture (resistor-ladder, delta-sigma, etc.).

2 Delta Sigma Conversion Revealed

- A delta sigma D/A converter "transforms" (i.e. requantizes) an N-bit PCM signal into a 1-bit signal.
- Why requantize to a lower resolution? Because a 1-bit output is extremely easy to implement in hardware and there are ways to make that one-bit output have the SNR of an *N*-bit converter.
- How do you get an N-bit-to-1-bit quantizer, which would normally only produce a 6 · 1 = 6 dB SNR, to produce the required 6N dB SNR? By using oversampling and noise-shaping to modify the 1-bit output.

3 Oversampling

- Quantization noise is assumed white and uniformly-distributed with a total power of $q^2/12$, where q is the quantization step-size.
- NOTE: The total quantization noise power does NOT depend on the sample rate!!!
- Quantization noise modeled as a noise source added to the signal:



Figure 1: Quantizer Model



Figure 2: Quantizer Transfer Function

The "in-band" quantization noise power can be reduced by sampling at a rate higher than Nyquist.



Figure 3: $2 \times$ Oversampled Quantization Noise Spectrum

Since the total in-band noise power is reduced, the number of "effective" bits is increased from the actual bits according to the relationship

$$M = 4^K,$$

where M is the oversampling factor and K is the number of extra bits.



Oversampling alone is an inefficient way to obtain extra bits of resolution. A gain of even a few bits would require astronomical oversampling ratios! We must use the additional technique of *noise-shaping* to make a 1-bit converter feasible.

4 Noise-Shaping

Shapes the oversampled quantization noise spectrum so that less noise is in-band:



Figure 5: Typical Noise-Shaped Spectrum

Noise-shaping is accomplished by placing feedback around the quantizer:



Figure 6: Classic First-Order Noise-Shaper

The transfer function of figure 6 is derived as follows:

$$W(z) = X(z) - z^{-1}Y(z)$$

$$\Sigma(z) = W(z) + z^{-1}\Sigma(z) \Longrightarrow \Sigma(z) = \frac{W(z)}{1 - z^{-1}}$$

$$Y(z) = \Sigma(z) + Q(z) = \frac{W(z)}{1 - z^{-1}} + Q(z)$$

$$1 - z^{-1}Y(z) = W(z) + (1 - z^{-1})Q(z)$$

$$= X(z) - z^{-1}Y(z) + (1 - z^{-1})Q(z)$$

$$Y(z) = X(z) + (1 - z^{-1})Q(z)$$
 (1)

It is clear from equation 1 that the signal X(z) passes through unmodified while the quantization noise Q(z) is modified by the term $1 - z^{-1}$. In delta-sigma modulator terminology this quantization noise coefficient is referred to as the *noise transfer* function [2], or NTF, denoted N(z). Thus $N(z) = 1 - z^{-1}$.



Figure 7: Noise Transfer Function Power Response of a First-Order Modulator

The noise-shaping can be made stronger by embedding integrator loops:



Figure 8: Second-Order Delta-Sigma Modulator

• The number of embeddings is termed the *order* of the modulator. An *L*th-order modulator has NTF

$$N(z) = (1 - z^{-1})^L.$$

• It can be shown [3] that the in-band quantization noise power relative to the maximum signal power as a function of oversampling ratio M and modulator order L is

$$\frac{6L+3}{2\pi^{2L}}M^{2L+1}.$$



Figure 9: Ratio of In-Band Quantization Noise Power To Signal Power versus Oversampling Ratio and Modulator Order L

5 Alternate Modulator Architecture

$$Y(z) = X(z) + (1 - z^{-1}H(z))Q(z).$$
(2)

To be equivalent with the classic architecture, H(z) = z - zG(z). Is H(z) realizable???



Figure 10: Alternate Delta-Sigma Modulator Architecture





Figure 11: Delta Sigma Modulator with Dither



Figure 12: Equivalent Dithered Modulator

6 Psychoacoustic Noise-Shaping

• The alternate architecture admits any NTF of the form

$$N(z) = 1 - z^{-1}H(z).$$

• The classic Lth-order modulator NTF contains L zeros at z = 1 (DC),

$$N(z) = \frac{(z-1)^L}{z^L}.$$

• When L is even we can use conjugate pairs to place the zeros at any L/2 frequencies on the unit circle.

Example: For L = 2, we can place the zero at any frequency f, $0 \le f \le MF_s/2$:



Figure 13: Zeros for Psychoacoustic Noise-Shaping, $\theta = \pi \frac{f}{MF_s}$.



Figure 14: NTF Power Response $|N(f)|^2$ of Psychoacoustically Noise-Shaped Modulator with f = 4 kHz

7 The Complete Modulator



Figure 15: Delta Sigma D/A Converter Block Diagram

8 References

References

- [1] Richard G. Lyons. Understanding Digital Signal Processing. Prentice Hall, second edition, 2004.
- [2] Steven R. Norsworthy, Richard Schreier, and Gabor C. Temes. Delta-Sigma Data Converters: Theory, Design, and Simulation. IEEE Press, 1997.
- [3] David Johns and Ken Martin. Analog Integrated Circuit Design. Wiley Publishers, 1997.